

Extraction of GO and diffraction components from Physical Optics in terms of line integrations of equivalent edge currents by Modified Edge Representation

Makoto Ando, Luis Rodriguez
Tokyo Institute of Technology
Dept. Electrical and Electronic Engineering
Tokyo, Japan

mando@antenna.ee.titech.ac.jp, lrodriguez@antenna.ee.titech.ac.jp

Abstract: *The surface to line integral reduction of PO currents by using Modified Edge Representation (MER) was empirically proposed (1989). For the observer without the Stationary Phase Point (SPP) on the scatterer, this reduction was reinforced mathematically (2001). Recently we showed, for the observer with SPP inside the scatterer surface, the MER line integration around the SPP gives GO terms(2004). In this talk, these are unified to conclude that MER line integration along the periphery and inner SPP, extracts the diffraction and GO components of PO surface integrals, respectively, irrespective of the observer position.*

1. Introduction

Physical Optics (PO) [1] is one of the most widely used methods for estimating the scattered electromagnetic fields at high frequency from surface S. PO performs the scattered field calculations by two well-defined steps. Firstly, the total induced currents are approximated in the Geometrical Optics (GO) sense, based upon the locality principle. Secondly, the scattered field is obtained when the currents are integrated over scatterer surface using the radiation integral. The scattered fields, thus obtained, are free of discontinuities and singularities on geometrical boundaries (Shadow - Reflection boundaries) and caustics as are usual the case with GO and Geometric Theory of Diffraction (GTD)[2]. On the other hand, the surface radiation integral becomes computationally heavy in the high frequency and for the large size of the scatterer and also, it hides the physical interpretation of the problem. Therefore, many works have been presented with the aim of reducing radiation integral to the line one, using asymptotic, exact or theoretic developments as shown in [3] – [6]. The reduction to line integral expressions also gives important and effective tools for the mechanism extraction of PO errors [7].

One of the complicated issues for surface to line integral reduction is “how to separate the diffraction and GO terms”. In asymptotic discussion with the base on the method of stationary phase, the line integration around the periphery of the scatterer is regarded as the diffraction components [8][9]. On the other hand, if the line integration is derived exactly based upon the Field equivalence theorem, it should be equivalent not to the diffraction but to the scattered or GO + diffraction components [4][5]. The GO contribution from the central part of the surface, if any, would also be expressed as if it emanated from the edge. The former is more natural than the latter in that the equivalent edge currents express the diffraction which is inherently generated at the edge; diffraction is believed to be local phenomenon and it seems possible to define the equivalent edge currents in terms of local parameters only. However, since the relation between the diffraction and the PO radiation integrals varies with the observation regions or the location of the stationary phase point (SPP) vs the integration area, the comparison between the line integration for diffraction and the PO surface integration is not straightforward.

Authors have empirically proposed unique concepts of equivalent edge currents for PO diffraction components, named Modified Edge Representation (MER) [9] [10]. It was mathematically reinforced for the observer which has no stationary phase point (SPP) on the surface of the scatterer [8]. Recently, MER line integration was conducted not only along the periphery of the scatterer, but also along the infinitesimally small contour around the SPP inside the surface of scatterer (SPP_i) if any [11]. It was numerically found that this gives the GO components.

This article summarizes these works and concludes two general observations for surface to line integral reduction in terms of MER.

- 1) MER line integration along the periphery corresponds to diffraction components of PO irrespective of observer position.
- 2) PO surface integration is decomposed into GO and diffraction terms, in terms of MER line integration along the infinitesimally small contour around SPP and along the periphery of the scatterer, respectively.

2. Modified Edge Representation for surface-to-line integral reduction

The scattering field E^S radiated from the surface currents is written as:

$$E^S = j \frac{k\eta}{4\pi} \iint_S \hat{r}_o \times (\hat{r}_o \times \bar{J}) \frac{e^{-jk r_o}}{r_o} dS \quad (1)$$

where r_o is the distance from the integration point S to the observer and $\hat{r}_o$ is the unit vector toward the observer. The time factor $e^{j\omega t}$ has been suppressed and only the $O(1/r_o)$ term is adopted assuming the observer is in the distance much larger than the wavelength. In PO, the surface electric current, $\bar{J}$ is approximated by $\bar{J} = 2\hat{n} \times H^i$ where $\hat{n}$ is the unit vector normal to the surface. The scattering field thus obtained is denoted by E_{PO} hereafter. The relation and the definition of PO scattering fields and diffracted fields are checked first. The scattered field is simply defined as total field minus incident field everywhere. PO surface integration is the approximation for the scattered field in this definition. On the other hand, the definition of diffracted fields (E^{diff}) varies with the observation positions in association with that of GO fields. The source and the scatterer define three regions in the space. Regions I and III are reflection and shadow region, respectively. The stationary phase points fall on the scatterer surface (SPP_i). Region II is the space for which SPP is outside of the surface (SPP_o). The diffracted field is related with PO radiation integral as in Table 1, where E^R and E^i indicate the GO reflection and the direct incident wave associated with SPP_i, respectively.

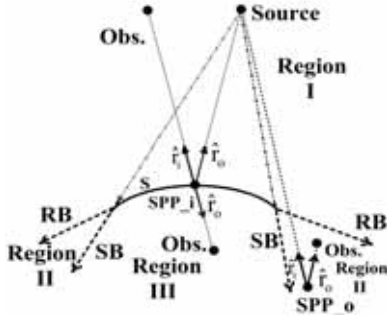


Figure 1 Scattering geometry and regions

Region	E_{PO}^{Diff}
Region I	$E_{PO} - E^R$
Region II	E_{PO}
Region III	$E_{PO} + E^i$

Table 1. Definition of diffraction field in each region

MER is the unitary vector ($\hat{\tau}$) defined to satisfy the diffraction law, at the point of interest, for given directions of incidence and observation. So, $\hat{\tau}$ may be calculated from:

$$(\hat{r}_i + \hat{r}_o) \cdot \hat{\tau} = 0 \quad (2)$$

$$\hat{n} \cdot \hat{\tau} = 0$$

Vector $\hat{\tau}$ depends on the source-observer directions as well as vector normal ($\hat{n}$) to the surface (local dependence). Figure 2 illustrates the MER vector $\hat{\tau}$ defined at each point on the edge as well as that inside the surface for the later extension. Figure 3 gives the example of MER and the visualized diffraction from the edge of the $15\lambda \times 15\lambda$ square plate. The source is a Hertzian electric dipole with moment $(1,0,0)$ located at $(0,0,5\lambda)$ and observer is at $(-3\lambda, 5\lambda, 15\lambda)$. The vector $\hat{\tau}$ changes its direction and coincides with the real edge, only at four diffraction points. The significance of MER is its use in the reduction of PO surface radiation integral to the line one. The equivalent electric and magnetic line currents along the actual edge $\hat{\tau}$ are defined using the modified edge $\hat{\tau}$ as follows.

$$M_l^{MER} = \frac{(\hat{r}_o \times -J_o) \times \hat{\tau}}{j(1 - (\hat{r}_o \times \hat{\tau})^2)(\hat{r}_i + \hat{r}_o) \cdot (\hat{\tau} \times \hat{n})} \hat{\tau} \quad (3) \quad J_l^{MER} = \frac{\{\hat{r}_o \times (\hat{r}_o \times J_o)\} \times \hat{\tau}}{j(1 - (\hat{r}_o \times \hat{\tau})^2)(\hat{r}_i + \hat{r}_o) \cdot (\hat{\tau} \times \hat{n})} \hat{\tau} \quad (4)$$

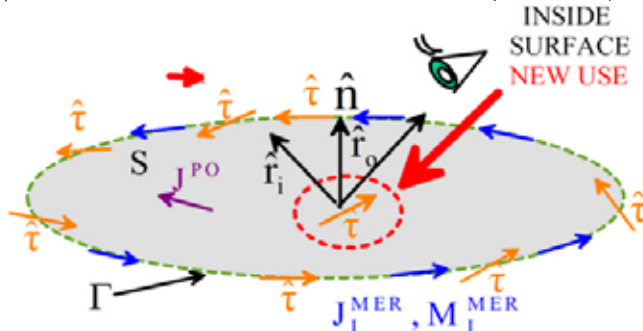


Figure 2 Definition of modified edge $\hat{\tau}$

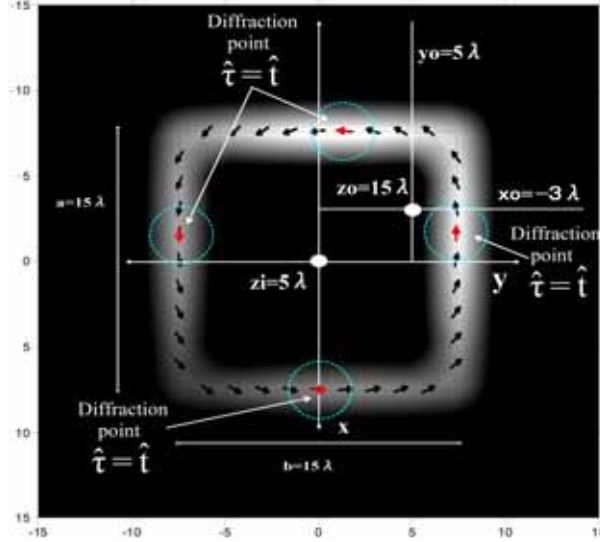


Figure 3 MER for a square plate

It is noted that J_1^{MER} and M_1^{MER} are singular at the SPPs on the edge if any; where $(\hat{r}_i + \hat{r}_o) \cdot (\hat{\tau} \times \hat{n}) = 0$

For region II, where there are no SPP_i, the Stokes theorem as well as the asymptotic approximation apply and it was mathematically proved that the PO surface radiation integral in (1) can be reduced to the MER^{Edge} line integrals as[8]:

$$\text{MER}^{\text{Edge}} \cong jk\eta(\bar{A} + \bar{B}) \quad (5)$$

where:

$$\begin{bmatrix} \bar{A} \\ \bar{B} \end{bmatrix} = \frac{k}{4\pi} \oint_{\Gamma} \begin{bmatrix} \hat{r}_o \times \hat{r}_o \times J_1^{\text{MER}} \\ \hat{r}_o \times M_1^{\text{MER}} \end{bmatrix} \frac{e^{-jk(r_i + r_o)}}{r_o} dl \quad (6)$$

The high accuracy of this integral reduction were demonstrated in [8] for flat and curved surfaces. Referring to the definition of diffraction in this region from Table 1, it comes that MER^{edge} corresponds to diffraction component of PO, denoted by MER^{diff} hereafter.

As for the regions I and III where SPPs exist on the scatterer surface, the MER currents are singular there as is illustrated in Figure 4 and the mathematical treatment based upon Stokes theorem in [8] is no longer valid. Furthermore, the entity of MER^{edge} is not clear. The recent work [11] extends the MER line integration along the periphery to that along the infinitesimally small contour around the SPP_i (MER^{SPP}) as is shown in Figure 5. It is noted that J_1^{MER} and M_1^{MER} are singular at the specular reflection points for region I or at the intersection point of direct incidence for region III, denoted by SPP_i in the figures. The line contour Γ' is introduced as the boundary between S' and S_o. The radius of S' is ρ' and the limit $\rho' \rightarrow 0$ is considered.

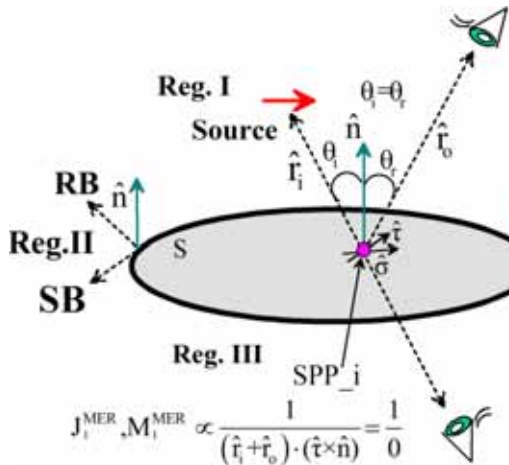


Figure 4 Position of Stationary Phase Point (SPP)

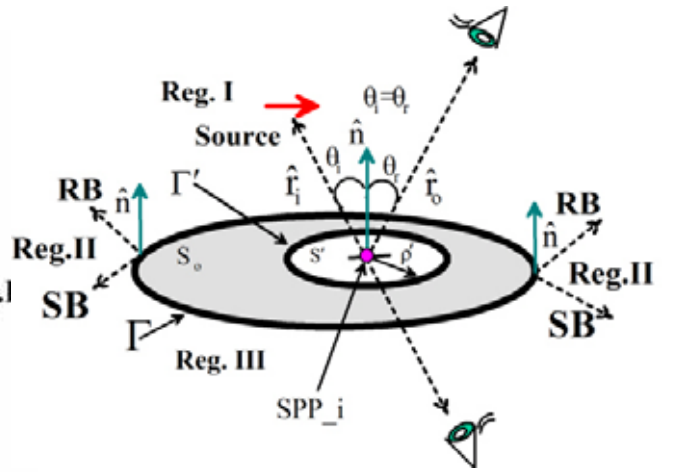


Figure 5 Surface to line integral reduction for region I or III.

The work [11] numerically showed that the line integration Γ' around the SPP gives E^R in region I while $-E^i$ in region III. Figure 6 shows the scattering geometry for a sphere where the contour for the line integration around the SPP at O with the radius ρ' is defined. Figure 7 shows in region I that as the contour becomes smaller ($1/\rho'$ becomes larger), MER^{SPP} is approaching to the value of GO reflection, which varies with the curvature ρ_s of the scatterer surface. We have confirmed also that in region III, MER^{SPP} converges to the direct incidence with opposite sign which precisely creates the geometrical shadow in the total field, irrespective of the surface curvature ρ_s .

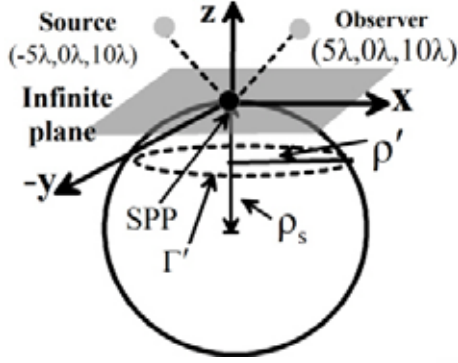


Figure 6-MER Line integration around SPP_i on a sphere

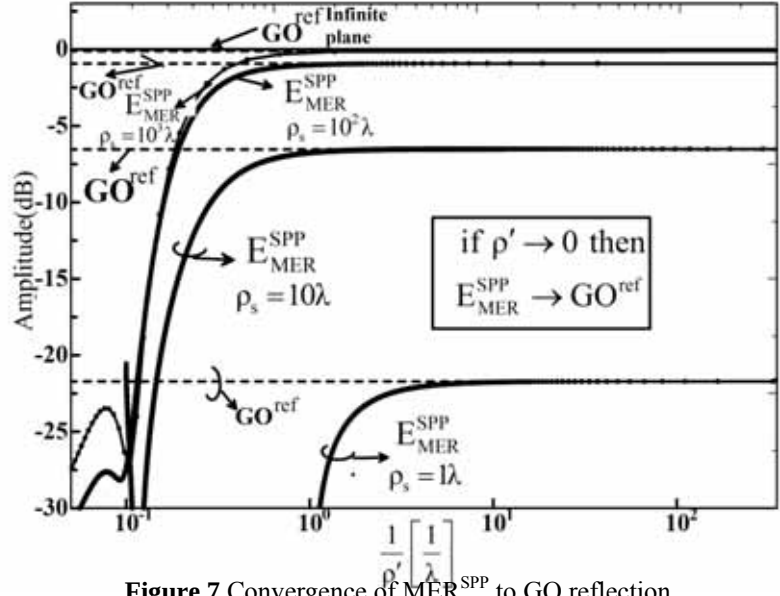


Figure 7 Convergence of MER^{SPP} to GO reflection

3. Extraction of GO and diffraction from PO surface integration in terms of MER line integrations. -Discussions -

In this section, the results in [8] for region II and those in [11] for region I and III are combined and their significance is highlighted. In region II, it was mathematically proved that the PO surface integration E_{PO} is reduced to MER line integration along the periphery (denoted by E_{MER}^{Per}) [8]. Since $E_{PO} = E^{diff}$ in region II from Table 1, we can conclude

$$E_{MER}^{Per} = E^{diff} \quad (\text{Region II}) \quad (7)$$

Then the surface to line integral reduction is discussed for regions I and III, with reference to Figure 5. To utilize the result in [8], the surface S will be divided into S' around the SPP_i, and the complementary one S_o . Now the surface to line integral reduction for S_o is considered. Since the PO currents are regular and finite everywhere, E_{PO} for S' vanishes and E_{PO} for S equals to E_{PO} for S_o . The result [8] is applied for S_o and we get

$$E_{PO} = E_{MER}^{Peri} + E_{MER}^{SPP} \quad (8)$$

The numerical results in [11] can be summarized as,

$$-E_{MER}^{SPP} = \begin{cases} -E^R & (\text{region I}) \\ E^i & (\text{region III}) \end{cases} \quad (9)$$

or with (8)

$$E_{PO} = E_{MER}^{Peri} \begin{cases} -E^R & (\text{region I}) \\ +E^i & (\text{region III}) \end{cases} \quad (10)$$

Then we get the unified expression from (7), (9) and (10) with reference to Table 1 as

$$E_{MER}^{Per} = E_{PO}^{diff} \quad (\text{every region}) \quad (11)$$

$$E_{MER}^{SPP} = E_{PO}^{GO} \quad (\text{if any}) \quad (12)$$

We conclude that PO surface integration is decomposed into two MER line integrations, where E_{MER}^{SPP} around the SPP_i and E_{MER}^{Per} along the periphery correspond to GO and diffraction, respectively. Furthermore the substance of E_{MER}^{Per} for regions I and III has been identified to be diffraction component for the first time; more simply E_{MER}^{Per} corresponds to PO diffraction everywhere.

4. Conclusions

In this article, the surface to line integrals reduction of PO is discussed. PO is decomposed into two MER line integrations corresponding to the GO and the diffraction. At the same time, MER line integration along the scatterer periphery corresponds to diffraction component in every region of observation.

5. References

- [1] R.F.Harrington: Time-Harmonic Electromagnetic Fields, p.127, McGraw-Hill, New York (1961)
- [2] E.Yamashita: Analysis Methods for Electromagnetic Wave Problems, p.131. Artech House (1990)
- [3] A. Rubinowicz: "The Miyamoto-Wolf diffraction wave", Progress in Optics, vol.4, pp.201-240, 1965
- [4] K. Miyamoto and E. Wolf: "Generalization of the Maggi-Rubinowicz theory of the boundary diffraction wave – Part I and Part II", J. Opt. Soc. Am., vol.52, pp.615-637, 1962.
- [5] J.S. Asvestas: "The physical optics fields of an aperture on an perfecting conducting screen in terms of line integrals", IEEE Trans. on Antennas and Propag., vol.AP-34, no.9, pp.1155-1159, Sept. 1986
- [6] P.M. Johansen and O. Breinbjerg, "An exact line integral representation of the physical optics scattered field: The case of an perfectly conducting polyhedral structure illuminated by electric herzian dipoles," IEEE Trans. on Antennas and Propag., vol.AP-43, no.7, pp.689-696, July, 1995.
- [7] P.Y.Ufimtsev: "Method of edge waves in the physical theory of diffraction", Prepared by the U.S. Air Force Foreign Technology Division Wright Patterson AFB, OHIO, 1971.
- [8] K. Sakina and M. Ando: "Mathematical derivation of modified edge representation for reduction of surface radiation integral," IEICE Trans. Electron., vol.E-84-C, no.1, pp.74-83, Jan. 2001.
- [9] T. Gokan, M. Ando and T. Kinoshita: "A New Definition of Equivalent Edge Currents in a Diffraction Analysis", IEICE Technical Report, AP89-64, dec. 1989.
- [10] T. Murasaki and M. Ando: "Equivalent edge currents by the modified edge representation: Physical Optics components", IEICE Trans. Electron, vol.E75-C, No.5, pp.617-626, 1992
- [11] L. Rodriguez and M. Ando: "GO field extraction from PO in terms of Modified Edge Representation (MER)". EMT Technical Meeting on Electromagnetic Theory, IEE Japan. EMT - 04-49-. pag 25. 2004

Makoto Ando was born in Hokkaido, Japan, in 1952. He received the B.S., M.S. and D.E. degrees in electrical engineering from Tokyo Institute of Technology, Tokyo, Japan in 1974, 1976 and 1979, respectively. From 1979 to 1983, he worked at Yokosuka Electrical Communication Laboratory, NTT, and was engaged in development of antennas for satellite communication. He was a Research Associate at Tokyo Institute of Technology from 1983 to 1985, and is currently a Professor.

His main interests have been high frequency diffraction theory such as Physical Optics and Geometrical Theory of Diffraction. His research also covers the design of reflector antennas and waveguide planar arrays for DBS and VSAT. Latest interest includes the design of high gain millimeter-wave antennas. He serves as the chairman of the technical program committee of ISAP(International Symposium on Antennas and Propagation) in 2000, the technical program Co-chair for the 2003 IEEE Topical conference on wireless communication technology, the Vice-Chair of ISAP 2004 and the Chair of 2004 URSI International Symposium on Electromagnetic Theory. He was the guest editor-in-chief of the special issue on “Innovation in Antennas and Propagation for Expanding Radio Systems” in IEICE Transactions on Communications in 2001.

He received the Young Engineers Award of IECE Japan in 1981, the Achievement Award and the Paper Award from IEICE Japan in 1993. He also received the 5th Telecom Systems Award in 1990 and the 8th Inoue Prize for Science in 1992. He serves as the Chair of Commission B of URSI since 2002. He is a member of administrative committee of IEEE Antennas and Propagation Society from 2004. He is a council of IEICE Japan. He is a Fellow of IEEE.

Makoto Ando 1952 yılında Hokkaido Japonya’da doğdu. Lisans, Yüksek Lisans ve Doktora derecelerini sırasıyla 1974, 1976 ve 1979 yıllarında Tokyo Institute of Technology’den (TIT) aldı. 1979’dan 1983 yılına kadar Yokosuka Elektrik İletişim Labaratuvarında uydu iletişimi için anten geliştirme konularında çalıştı. 1983-1985 yılları arasında araştırmacı olarak TIT’de bulundu. Şu anda TIT’de Profesörlük yapmaktadır.

Dr. Ando’nun çalışma alanları Fiziksel Optik ve Kırınımın Geometrik Teorisi gibi yüksek frekans teknikleri üzerinedir. Ayrıca DBS ve VSAT için yansıtıcı antenler ve dalgakılavuzlu düzlemsel dizili antenler konusunda da çalışmaktadır. Son araştırması yüksek kazançlı milimetrik-dalga anten konularındadır. 2000 yılı Uluslararası Antenler ve Yayınım Sempozyumunun (ISAP) teknik program komitesinin başkanlığı, 2003 IEEE Haberleşme Teknolojisi konferansının başkan yardımcılığı, 2004 URSI Elektromanyetik Teori Uluslararası Konferansı başkanlığı görevlerini üstlenmiştir. 2001 yılında “Gelişen Radyo Sistemleri için Antenler ve Yayınımındaki Yenilikler” konusunda IEICE dergisinde misafir editörlük yapmıştır.

1981 yılında IEICE Genç Mühendisler ödülü, 1993 yılında IEICE Japonya Başarı Ödülü ve IEICE Makale ödülleri almıştır. Ayrıca 1990 yılında 5. Telekom Sistemleri Ödülü ve 1992 yılında 8. Inoue Bilim Ödülünü almaya hak kazanmıştır. 2002 yılından beri URSI B Komitesi başkanıdır. 2004 yılından bu yana IEEE Antenler ve Yayınım Topluluğunun idari komitesindedir. IEICE Japonya konsey üyesi ve IEEE Fellow üyesidir.